

*[Water Resources Research]*

Supporting Information for

**[Global runoff partitioning based on Budyko-constrained machine learning]**[Shujie Cheng<sup>1,2</sup>, Petra

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# 1 Method

## Baseflow curve based on limit concept

In general, the water balance can be written as:

$$\frac{dS}{dt} = P - E_a - Q \quad (S1)$$

where  $S$  is water stored in underground,  $P$  is precipitation,  $E_a$  is actual evaporation,  $Q$  is discharge which can be partitioned into  $Q_b$  is baseflow and  $Q_q$  is quick flow ( $Q = Q_b + Q_q$ ).

The basic limit concept of the Budyko framework for estimating  $E_a$  is:  $E_a/P \rightarrow 1$  as  $E_p/P \rightarrow \infty$  for very dry conditions, and  $E_a \rightarrow E_p$  as  $E_p/P \rightarrow 0$  for very wet conditions, where  $E_p$  is potential evaporation. The demand limit of  $E_a$  is  $E_p$  and the supply limit is  $P$ . Fu (1981) proposed  $E_a$  can be calculated with:

$$\frac{E_a}{P} = 1 + \frac{E_p}{P} - \left[1 + \left(\frac{E_p}{P}\right)^{a_1}\right]^{1/a_1} \quad (S2)$$

Assuming  $\frac{dS}{dt} \approx 0$  on long term time scales and with the catchment retention defined as

$$CR = E_a + Q_b \quad (S3)$$

Equation S1 can be expressed as:

$$P = CR + Q_q \quad (S4)$$

The demand limit for  $CR$  is  $CR_0 = E_p + Q_{b,p}$ . The  $E_p$  and  $Q_{b,p}$  are the potential values for  $E$  and  $Q_b$ , respectively. According to Zhang et al. (2008), the limits concept of Budyko can also be applied to  $CR$  such that:  $CR/P \rightarrow 1$  as  $CR_0/P \rightarrow \infty$  for very dry conditions, and  $CR \rightarrow CR_0$  as  $CR_0/P \rightarrow 0$  for very wet conditions. Then  $CR$  can be estimated as:

$$\frac{CR}{P} = 1 + \frac{CR_0}{P} - \left[1 + \left(\frac{CR_0}{P}\right)^{a_2}\right]^{1/a_2} \quad (S5)$$

Combining Eq. S2, Eq. S3 and Eq. S5:

$$\frac{Q_b}{P} = \frac{Q_{b,p}}{P} + \left[1 + \left(\frac{E_p}{P}\right)^{a_1}\right]^{1/a_1} - \left[1 + \left(\frac{E_p + Q_{b,p}}{P}\right)^{a_2}\right]^{1/a_2} \quad (S6)$$

Under very limited storage capacity conditions (for instance an impervious catchment), no/limited water is stored in the subsurface such that the baseflow also approaches zero (i.e.,  $Q_b/P \rightarrow 0$  if  $Q_{b,p}/P \rightarrow 0$ ). Under that condition, Eq. S11 changes to  $0 \approx \left[1 + \left(\frac{E_p}{P}\right)^{a_1}\right]^{1/a_1} - \left[1 + \left(\frac{E_p}{P}\right)^{a_2}\right]^{1/a_2}$ .

This equation can only be satisfied if  $a_1 = a_2$ . Thus Eq. S11 can be written as:

$$\frac{Q_b}{P} = \frac{Q_{b,p}}{P} + \left[1 + \left(\frac{E_p}{P}\right)^\alpha\right]^{1/\alpha} - \left[1 + \left(\frac{E_p + Q_{b,p}}{P}\right)^\alpha\right]^{1/\alpha} \quad (S7)$$

## 2 Figures

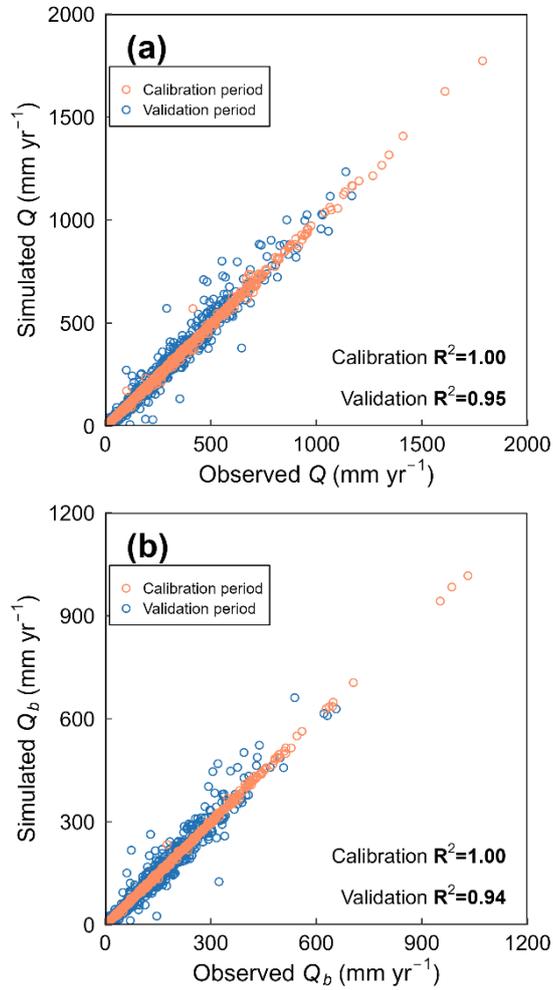


Figure S1. Performance of (a)  $Q$  and (b)  $Q_b$  at catchment scale during the calibration (orange) and validation (blue) periods.

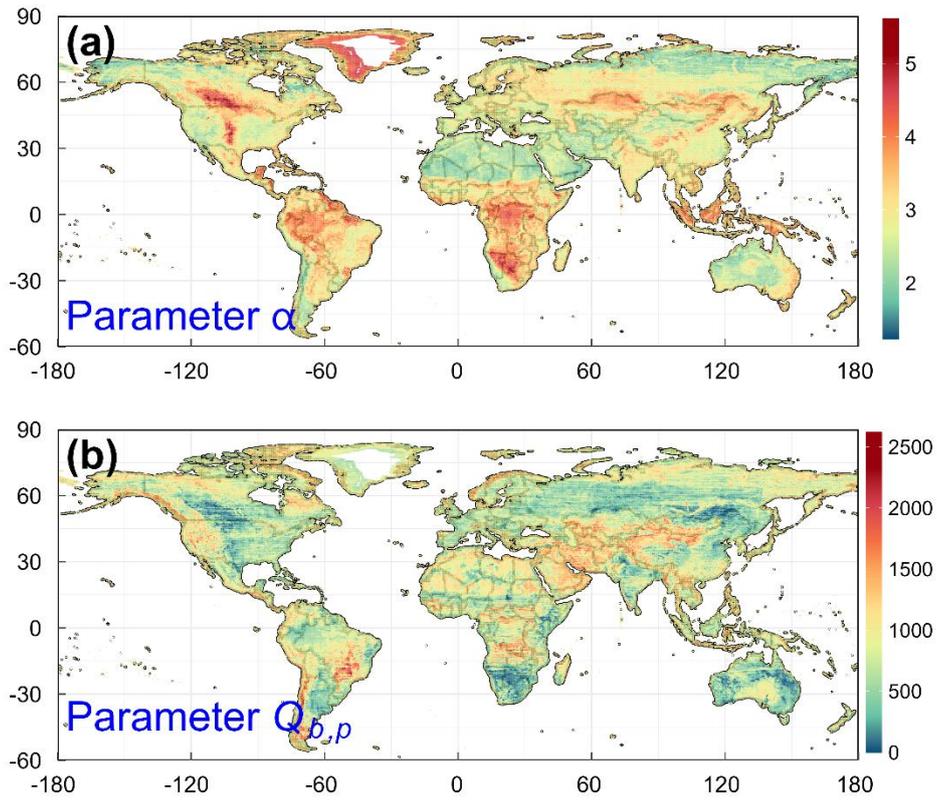


Figure S2. Global maps of (a) parameter  $\alpha$  in the Budyko curve (Eq. 3) and BFC curve (Eq. 4), and (b) parameter  $Q_{b,p}$  in BFC curve estimated as the mean of 10 BRT models.

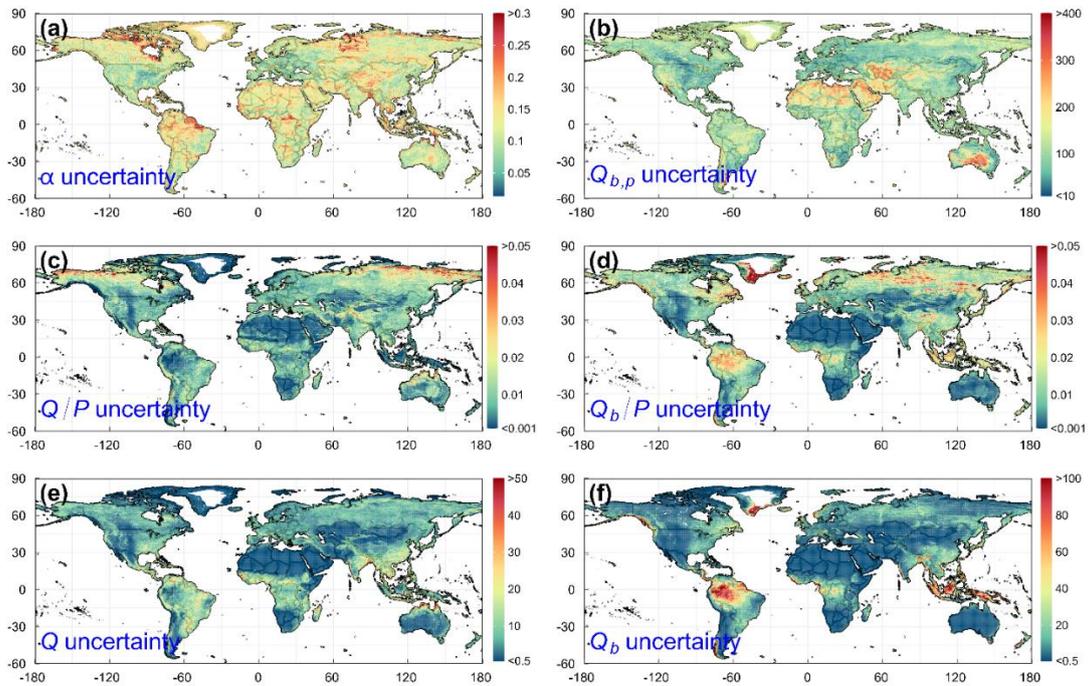


Figure S3. Global map of the uncertainty of (a) parameter  $\alpha$ , (b) parameter  $Q_{b,p}$ , (c) runoff coefficient ( $RC=Q/P$ ), (d) baseflow coefficient ( $BFC=Q_b/P$ ), (e) runoff ( $Q$ ), and (f) baseflow ( $Q_b$ ). These uncertainty values are equal to the standard deviation of the 10 trained BRT models using the 10-fold cross-validation strategy.

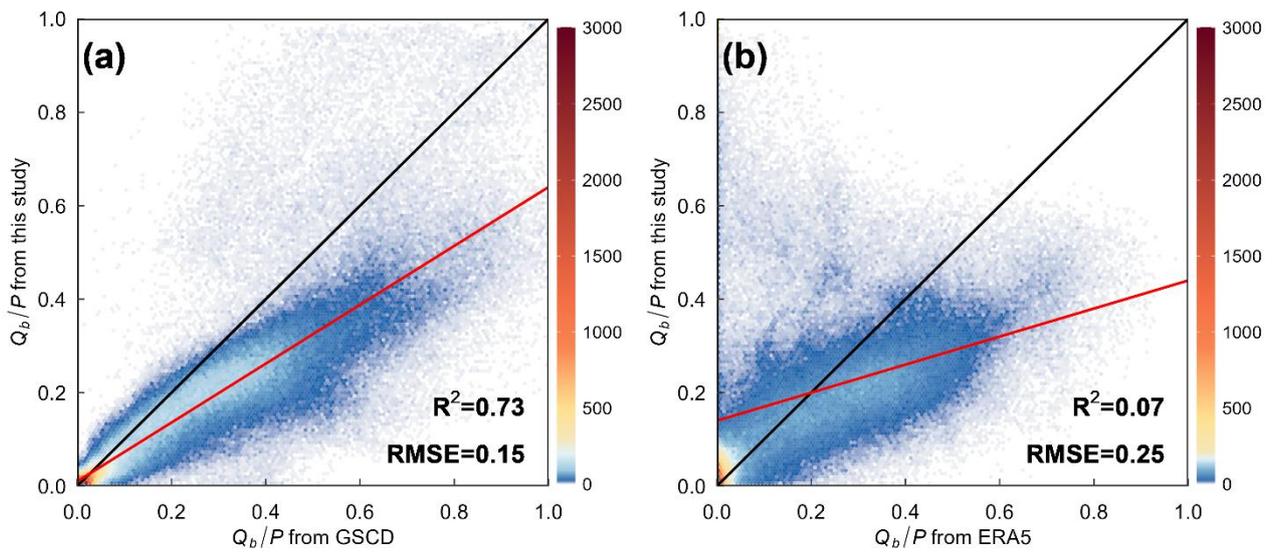


Figure S4. Comparison of the baseflow coefficient ( $Q_b/P$ ) from this study with estimates according to (a) GSCD and (b) ERA5-Land.

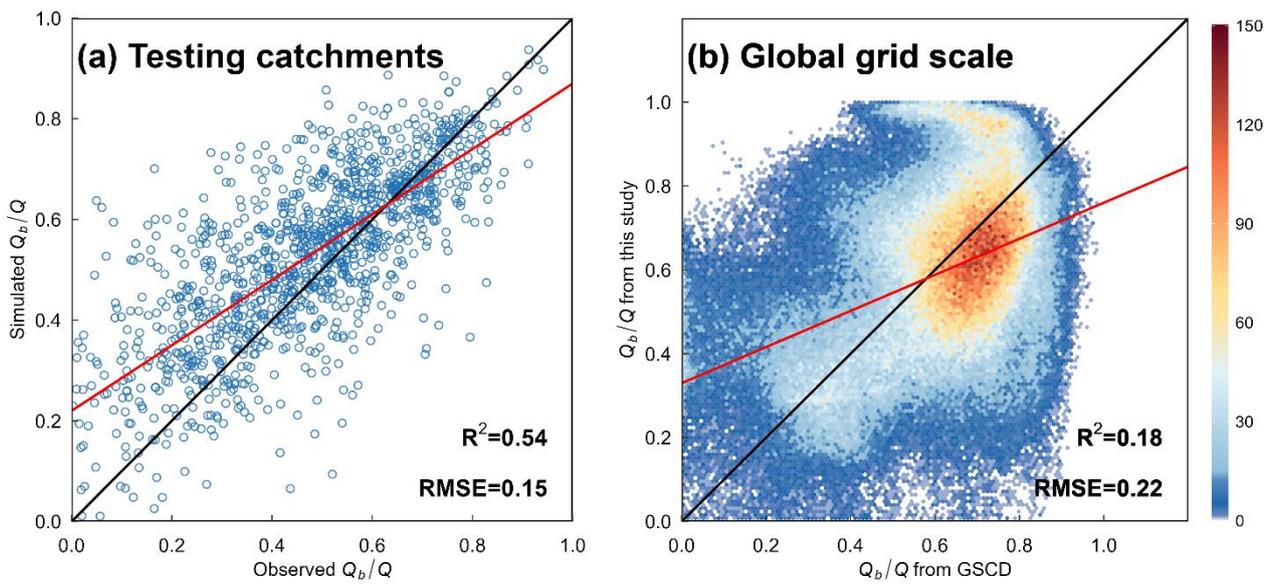


Figure S5. Comparison of the baseflow index ( $Q_b/Q$ ) as estimated in this study with (a) field observations and (b) GSCD estimates.