Optimized recess etching criteria for T-gate fabrication achieving $f_t=290$ GHz at $L_g=124$ nm in metamorphic HEMT with In_{0.7}Ga_{0.3}As channel

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April 14, 2023

Abstract

We propose criteria for recess etching to fabricate T-gate used in InGaAs HEMTs. By patterning additional rectangular pads on the source and drain metals in the e-beam lithography step, it is possible to measure the drain-to-source resistance (R_{ds}) and current (I_{ds}) . the ratio (Γ) of before and after etching for each R_{ds} and I_{ds} can be used as criteria to determine the point in time to stop etching. By performing recess etching with $\Gamma = 1.97$ for R_{ds} and $\Gamma = 0.38$ for I_{ds} on an epiwafer having cap doping concentration of $2 = 10^{19}$ cm⁻³ and channel indium content of 0.7, we have fabricated InGaAs mHEMT device showing $g_{m,max} = 1603$ mS/mm and $f_t = 290$ GHz at $L_g = 124$ nm. The criteria presented can be applied to InGaAs HEMTs with various epitaxial structures.

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We propose criteria for recess etching to fabricate T-gate used in InGaAs HEMTs. By patterning additional rectangular pads on the source and drain metals in the e-beam lithography step, it is possible to measure the drain-to-source resistance (R_{ds}) and current (I_{ds}) . the ratio (Γ) of before and after etching for each R_{ds} and I_{ds} can be used as criteria to determine the point in time to stop etching. By performing recess etching with $\Gamma = 1.97$ for R_{ds} and $\Gamma = 0.38$ for I_{ds} on an epiwafer having cap doping concentration of 2×10^{19} cm⁻³ and channel indium content of 0.7, we have fabricated InGaAs mHEMT device showing $g_{m,max} = 1603$ mS/mm and $f_t = 290$ GHz at $L_g = 124$ nm. The criteria presented can be applied to InGaAs HEMTs with various epitaxial structures.

Introduction: Metamorphic high electron mobility transistor (mHEMT) with InGaAs channel material based on GaAs substrate can be applied to monolithic microwave integrated circuit (MMIC) with high frequency [1,2]. Compared to the competing InP-based InGaAs HEMT [3,4], the mHEMT exhibits relatively lower performance but is more cost-effective due to cheaper substrate price, the ability to fabricate on larger wafers, and ease of handling [5]. Both InP-based HEMT and GaAs-based mHEMT can have various epitaxial structures, mainly differentiated by the presence or absence of an InP layer between the cap and barrier layers. Here the InP layer acts as an etch stop layer during recess etching process. After finishing recess etching, gate metal stacks of Pt/Ti/Pt/Au are usually deposited on InP layer [6] or InAlAs barrier [7]. In this case, however, it is essential to optimize parameters such as the thickness of the bottom Pt layer and Pt sinking temperature [8]. On the other hand, not using an InP etch stop layer can avoid such issues, but there is a risk of etching into the channel during recess etching process. To solve this problem, it is necessary to measure the drain-to-source resistance (R_{ds}) and current (I_{ds}) before and after etching to find proper time to stop etching process. It can be done by developing additional recess pads on source and drain metals, which are coated by e-beam resists. In our previous works, we dealt with the uneven recess etch rate between fingers in multi-finger mHEMT [9] and the etching depth variation according to the foot width of the T-gate [10].

In this paper, we present criteria of performing citric acid-based electrochemical recess etching before T-gate metal evaporation to fabricate high-performance InGaAs HEMTs. We describe the fabrication process from mesa isolation to e-beam lithography for T-gate pattern formation, followed by the recess etching process. Based on the measurement results of transconductance (g_m) and cut-off frequency (f_t) , we emphasize the importance of the ratios (Γ) of before and after etching for R_{ds} and I_{ds} , which are criteria for optimization of recess etching. These criteria can be applied to InGaAs HEMTs with various epitaxial structures.

Fabrication process before recess etching: To fabricate InGaAs HEMT device, we used 4-inch GaAs substrate and molecular beam epitaxy (MBE) to grow epitaxial structures as shown in Table 1. First, metamorphic buffer layer, which was used to offset the lattice mismatch between GaAs and In_{0.52}Al_{0.48}As buffer layer, was grown on semi-insulating GaAs substrate by changing its In content (x) from x = 0 to 0.52. Then, In_{0.7}Ga_{0.3}As of 10 nm was formed to be used as a channel on In_{0.52}Al_{0.48}As buffer layer of 300 nm. The carrier density and channel mobility ($\mu_{S\eta}$) were 2.9×10^{12} cm² and 10710 cm²/V[?]s, respectively. Next, Si δ -doping of 6×10^{12} cm⁻² was applied to supply electrons to the channel upon In_{0.52}Al_{0.48}As spacer of 3 nm. Another Si δ -doping of 5.5×10^{12} cm⁻² was applied in In_{0.52}Al_{0.48}As barrier to enhance conductivity. Finally, In_{0.53}Ga_{0.47}As cap layer of 20 nm doped with Si of 2×10^{19} cm⁻³ was formed on In_{0.52}Al_{0.48}As barrier to fabricate Ohmic contacts of source and drain electrodes. The epitaxial structure designed by our research group was produced by IntelliEPI Inc. and its sheet resistance was 77.8 Ω /sq. By using this 4-inch epiwafer, mesa isolation was firstly conducted. Each HEMT device were separated by mesa having thickness of 200 nm, which were etched by solution of H₃PO₄:H₂O₂:H₂O= 1:1:40. As a result of transmission line measurement (TLM) with a gap of 5 µm between 100×100 µm mesa pads, 61 G Ω was measured, and 65 pA was flowed at 2 V, which confirms that mesa-to-mesa isolation was properly achieved.

Table 1: Epitaxial structure of InGaAs HEMT.

Layer	Material	THK	Level	Type
cap	$In_{0.53}Ga_{0.47}As$	20 nm	$2.0 \times 10^{19} / \text{cm}^3$	N+
barrier	$In_{0.52}Al_{0.48}As$	2 nm	-	i
1^{st} δ -doping	Si	-	$5.5 \times 10^{12} / \text{cm}^2$	Ν
barrier	$In_{0.52}Al_{0.48}As$	6 nm	-	i
2^{nd} δ -doping	Si	-	$6.0 \times 10^{12} / \mathrm{cm}^2$	Ν
spacer	$In_{0.52}Al_{0.48}As$	$3 \mathrm{nm}$	-	i
channel	$In_{0.7}Ga_{0.3}As$	10 nm	-	i
buffer	$In_{0.52}Al_{0.48}As$	300 nm	-	i
m-buffer	GaAs -In $_{0.52}$ Al $_{0.48}$ As	300 nm	-	i

To fabricate Ohmic contact serving as a source and drain, Mo/Ti/Pt/Au, each with thickness of 10/30/30/280 nm, was deposited by using e-beam evaporator. The source-to-drain distance of the device was designed to be 2 µm. Also, the device was designed as a two-finger T-gate with a total gate width of 100 µm. To measure the resistance of Ohmic contact, patterns with interval of 5/10/20/40/80 µm were made. As a result of TLM measurement, a contact resistance (R_c) of 0.078 Ω [?]mm was measured.

After coating PMMA-based tri-layer to make T-gate patterns, e-beam lithography using Raith EBPG 5000 was performed with 100 nm target for foot and 600 nm target for head, respectively. In addition, "anchor" and "gate pad" were added to the end of each T-gate pattern to ensure structural stability, as shown in Fig. 1a. After finishing to develop patterns, descum process was performed to remove residues so that the final foot width became about 120 nm.



$a \ b$

Fig. 1 Top views of design for HEMT device.

a Anchor and gate pad added to the end of two-finger T-gate.

b Recess pads for monitoring R_{ds} and I_{ds} during recess etch process.

Gate recess etching: Before evaporating T-gate metal stacks, recess etching for InGaAs and InAlAs makes it possible to improve gate controllability so that higher g_m is secured. As shown in Fig. 1b, rectangular pads were additionally exposed on the source and drain metals in the e-beam lithography step [9,10]. These "recess pads" should have a size enough to contact probe tips. By using developed recess pads, it is possible to monitor R_{ds} and I_{ds} for biased drain voltage (V_D). Accordingly, it is feasible to find optimal point in time to stop etch and keep from etching of 2nd Si δ -doping layer on the In_{0.52}Al_{0.48}As spacer. Also, by using citric acid-based etchant, InGaAs/InAlAs layers can be electrochemically etched because potential difference occurs between InGaAs/InAlAs layer opened by foot pattern and Ohmic metal opened by recess pad. In the same way as our previous paper [10], an etchant comprising citric acid (10 g), hydrogen peroxide (1 ml), and water (430 ml) was used and maintained its temperature at 32 C°.

To find an appropriate point in time to stop etching, we compared the experimental results for two different epitaxial structures, which have the same thickness of $In_{0.53}Ga_{0.47}As$ cap and $In_{0.52}Al_{0.48}As$ barrier/spacer, but differ in cap doping concentration (N_{cap}), the number of Si δ -doping layers, and In content of channel. Figure 2 shows the R_{ds} at $V_d = 0$ V and the I_{ds} at $V_d = 1$ V for these two epitaxial structures. Comparing R_{ds} and I_{ds} before etching for $N_{cap} = 1 \times 10^{19} \text{ cm}^{-3}$ (dash-dotted line, [10]) and $N_{cap} = 2 \times 10^{19} \text{ cm}^{-3}$ (solid line, this work), high N_{cap} reduces R_{ds} and increases I_{ds} . The R_{ds} gradually increases as the thickness of the cap layer decreases by recess etching. Even if the cap layer is completely etched and InAlAs barrier is revealed, R_{ds} does not change abruptly and keep gradually increasing because Si δ -doping layers supply electrons to form current path.

In the previous work, we stopped to etch when $R_{ds} = 18.7 \ \Omega$ and $I_{ds} = 31.3 \ \text{mA}$ were measured, and the resultant device showed good performance [10]. Here the ratios (Γ) of before and after etching for each R_{ds}

and I_{ds} can be defined in equations as follows:

, , (1)

where i = 0, 1, 2..., n is integer and n means the number of times etching has been performed. In the case of previous work, $\Gamma_R = 1.82$ and $\Gamma_I = 0.39$. Referring to these ratios, in this work, etching was stopped when $R_{ds} = 13 \ \Omega$ and $I_{ds} = 34.7$ mA so that $\Gamma_R = 1.97$ and $\Gamma_I = 0.38$. Here, the Γ_R was adjusted slightly higher and the Γ_I was adjusted slightly lower, taking into consideration the additional 1st Si δ -doping layer and 0.7 of channel In content. Additionally, for another wafer with the same epitaxial structure as this work, more etching was carried out, resulting in a rapid change of $R_{ds} = 21.1 \ \Omega$ and $I_{ds} = 24.3 \ \text{mA}$ (dotted line) so that $\Gamma_R = 3.34$ and $\Gamma_I = 0.26$, which can be assumed to indicate etching down to the 2nd Si δ -doping layer. This led to a poor device operation of $I_{on} \ 10\text{mA}$ at $V_d = 0.8 \ \text{V}$ and $g_m \ 200 \ \text{mS/mm}$.



$a \ b$

Fig. 2 Measurement results of R_{ds} and I_{ds} for mHEMTs having cap layer of $N_{cap} = 1 \times 10^{19}$ cm⁻³ and $N_{cap} = 2x10^{19}$ cm⁻³ before and after recess etching process.

 $a R_{ds}$ when biasing $V_d = 0$ V.

 $b I_{ds}$ when biasing $V_d = 1$ V.

Following the etching process, the gate stack of Ti/Au= 40/400 nm were evaporated. After finishing lift-off process, SiN of 50 nm was deposited by PECVD for passivation. Figure 3 shows the results of transmission electron microscopy (TEM) using Tecnai F30 S-Twin after completing T-gate fabrication. The final gate length (i.e., gate foot width) is evaluated as about 124 nm (see Fig. 3a), which is similar to the length examined by CDSEM after descum. By magnifying TEM to make the epitaxial structures more visible, it can be observed that $In_{0.7}Ga_{0.3}As$ channel on $In_{0.52}Al_{0.48}As$ buffer has thickness of 10 nm, as designed (see Fig. 3b). Above the channel, it is noticeable that the thickness of $In_{0.52}Al_{0.48}As$ remaining after recess etching is about 7.7 nm. This means that the T-gate was deposited on 4.7 nm from the 2nd Si δ -doping layer, so it can be evaluated that the recess etching was properly performed to suppress the occurrence of gate leakage current.



$a \ b$

Fig. 3

Cross-sectional TEM images.

a T-gate foot deposited on recessed $In_{0.52}Al_{0.48}As$ layer.

b Magnified TEM image showing epitaxial structures below T-gate foot.

Electrical characteristics: Figure 4 illustrates the device performances by measuring with Keysight HP4142 and Cascade on-wafer probe station. During the measurement, the biased drain voltage (V_d) was fixed at 0.8 V. As shown in Fig. 4a, when gate voltage (V_g) was biased at -1 V, drain current (I_d) was measured at 1.6 μ A/mm. When biasing $V_g = 0.2$ V, the I_d was measured at 664.7 mA/mm. From the measurement results, the threshold voltage (V_{th}) and maximum transconductance ($g_{m,max}$) of -0.47 V and 1603 mS/mm were extracted, respectively. Subsequently, the S-parameter for the frequency range of 0.5-50 GHz was measured using a Keysight N5245A microwave network analyzer while $V_g = 0$ V and $V_d = 0.8$ V were applied to the same device. The result of calculating the current gain of h_{21} was shown in Fig. 4b. By extrapolating with a line of -20 dB/decade, 290 GHz of f_t was extracted.



Fig. 4 Electrical characteristics of mHEMT.

a Measured V_q - I_{ds} plot and extracted g_m curve at $V_d = 0.8$ V.

b Calculated h_{21} and extrapolated line to find f_t .

Figure 5 describes comparison between these results (f_t and $g_{m, max}$) and the other values reported by various research groups. All references dealt with mHEMTs for channel In x range from 0.6 to 0.8. Firstly, we obtained higher cut-off frequency of 290 GHz at longer gate length of 124 nm compared to the results of our previous work ($f_t = 210$ GHz at $L_g = 100$ nm, [2]). Considering that recess etching was carried out properly for both devices, the one of the main reasons for the difference in performance is epitaxial structure changed its channel In content from 0.6 to 0.7 and N_{cap} from $N_{cap} = 1 \times 10^{19} \text{ cm}^{-3}$ to $N_{cap} = 2 \times 10^{19} \text{ cm}^{-3}$.

Next, in comparison with the results from other research groups, the $f_t = 290$ GHz obtained in this paper is higher than that of devices with $L_g = 100$ nm [11] and $L_g = 80$ nm [7], which have f_t values of 220 GHz and 246 GHz, respectively. Also, the f_t performance in this paper is comparable to the device reporting $f_t =$ 293 GHz at $L_g = 70$ nm [12]. To analyse the reasons, it is necessary to perform a detailed analysis for each case because different epitaxial structures or device designs were used by each research group. However, a simple overview of all cases reveals that, as shown in Fig. 5b, our result shows relatively high $g_{m,max} = 1603$ mS/mm, which leads to the high f_t value according to the equation of $f_t = g_m / 2\pi (C_{gs} + C_{gd})$. Hence, it can be evaluated that the optimal recess etching performed in this study led to a sufficient g_m potentially achievable by the device design and epitaxial structure.



$a \ b$

Fig. 5 Comparison our results in this paper with other reported values for mHEMTs with In x range of 0.6-0.8.

a L_q - f_t plot for results comparison.

 $b L_g - g_{m,max}$ plot for results comparison.

Conclusion: We have demonstrated the recess etching technique for T-gate fabrication in InGaAs mHEMTs. By opening additional recess pads on the source and drain metals, it is possible to find the optimal point in time to stop etching by measuring R_{ds} and I_{ds} . Specifically, by referring the criteria of $\Gamma_R = 1.82$ and Γ_I = 0.39 for epiwafer having $N_{cap} = 1 \times 10^{19} \text{cm}^{-3}$ and channel In x = 0.6, we have adjusted the criteria and performed recess etching to be $\Gamma_R = 1.97$ and $\Gamma_I = 0.38$ for epiwafer having $N_{cap} = 2 \times 10^{19} \text{cm}^{-3}$ and channel In x = 0.7. As a result, we have fabricated mHEMT device showing $g_{m,max} = 1603 \text{ mS/mm}$ and $f_t = 290$ GHz at $L_g = 124$ nm. Even with different epitaxial structures, referring to the criteria of Γ_R and Γ_I ratios presented in this paper would be helpful to find the appropriate timing to stop recess etching for successful fabrication of InGaAs HEMTs.

Acknowledgments: This research was financially supported by the Institute of Civil Military Technology Cooperation funded by the Defence Acquisition Program Administration and Ministry of Trade, Industry and Energy of Korean government under grant No. 22-CM-TN-15.

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